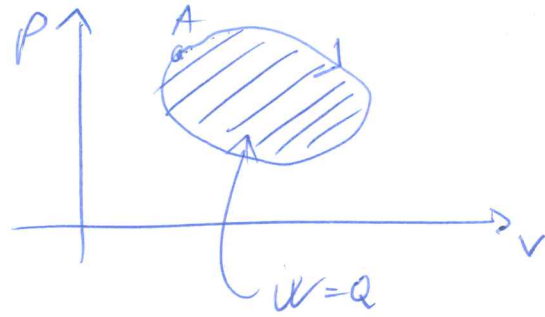


Trasformazioni cicliche

"Banalmente" primo principio si applica anche se stato iniziale = stato finale

$$\Rightarrow \Delta U = 0$$

$$\Rightarrow Q = W$$



curva chiusa P-V

senso orario \rightarrow W positivo

(c_p più alta in espansione, più bassa compressione)

senso antiorario \rightarrow W negativo

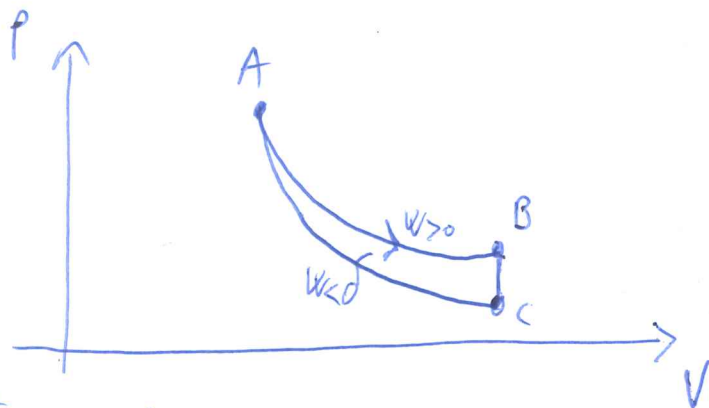
①
Esempio: IT-IC-AD

$$P_A, V_A, T_A \xrightarrow{\text{isoterma quasistatica}} P_B, V_B, T_B = T_A$$

adiabatica

$$P_C, V_C = V_B, T_C$$

isoterma quasistatica



Isoterma $A \rightarrow B$

$$\Delta U_{AB} = 0 \quad [\text{dato che } T_A = T_B \text{ e } U = U(T)]$$

$$W_{AB} = nR \ln\left(\frac{P_A}{P_B}\right) T_A \quad Q_{AB} = W_{AB}$$

$$Q_{AB}, W_{AB} > 0$$

Isocora $B \rightarrow C$

$$\Delta U_{BC} = n c_v (T_C - T_B) = n c_v (T_C - T_A)$$

$$W_{BC} = 0$$

$$Q_{BC} = \Delta U_{BC}$$

$$T_C \approx \frac{P_C V_C}{nR} <$$

$$T_A = \frac{P_A V_A}{nR}$$

$$T_B = \frac{P_B V_B}{nR}$$

$$T_C < T_A, T_B$$

Adiabatica C → A

$$\Delta U_{CA} = nC_V(T_A - T_C)$$

$$W_{CA} = -\Delta U_{CA} \quad Q_{CA} = 0 \quad W < 0, \Delta U > 0$$

→ nota: serve scelta particolare di R affinché $P_A V_A^\gamma = P_C V_C^\gamma$

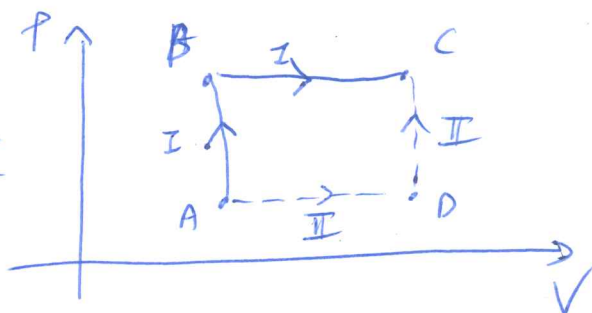
lungo il ciclo

$$\Delta U = 0 + nC_V(T_C - T_A) + nC_V(T_A - T_C) = 0 \quad ! \quad \text{Come dovrebbe essere}$$

$$W = nRT_A \ln\left(\frac{P_A}{P_B}\right) + nC_V(T_A - T_C)$$

$$Q = nRT_A \ln\left(\frac{P_A}{P_B}\right) + nC_V(T_C - T_A) + 0 = -W \quad ! \quad \text{Come dovrebbe essere}$$

Esempio: IC/IC-IB



Consideriamo prima A → B → C

Isocora A → B
~~A → B~~

$$\frac{P_B}{P_A} = \alpha > 1$$

$$T_A = \frac{P_A V_A}{nR} \rightarrow T_B = \frac{P_B V_B}{nR} = \alpha T_A$$

$$\Delta U_{AB} = nC_V \Delta T_{AB} = nC_V T_A (\alpha - 1)$$

$$W_{AB} = 0 \quad (\text{in quanto } \Delta V = 0)$$

$$Q = nC_V \Delta T_{AB} = nC_V T_A (\alpha - 1) = \Delta U_{AB} > 0$$

Isobara B → C

$$\frac{V_C}{V_B} = \beta > 1$$

$$P_C = \frac{nRT_C}{V_C}$$

$$P_B = \frac{nRT_B}{V_B} \rightarrow P_C = P_B \quad T_C = \beta T_B$$

$$Q_{BC} = nC_P(T_C - T_B) = nC_P T_B (\beta - 1) = nC_P T_A \alpha (\beta - 1)$$

$$W_{BC} = P_B(V_C - V_B) = nR(T_C - T_B) = nRT_B(\beta - 1) = nRT_A \alpha (\beta - 1)$$

$$\Delta U_{BC} = nC_V(T_C - T_B) = nC_V T_B (\beta - 1) = nC_V T_A \alpha (\beta - 1) = Q_{BC} - W_{BC} \quad \text{in quanto } C_V = C_P - R$$

Compressivamente

$$\Delta U_{AC}^I = \Delta U_{AB} + \Delta U_{BC} = n c_v T_A (\alpha - 1) + n c_v T_A \alpha (\beta - 1) = n c_v T_A (\alpha \beta - 1)$$

$$Q_{AC}^I = n c_v T_A (\alpha - 1) + n c_p T_A \alpha (\beta - 1) = n T_A [c_v (\alpha - 1) + c_p \alpha (\beta - 1)]$$

$$W_{AC}^I = 0 + n R T_A \alpha (\beta - 1) = n R T_A \alpha (\beta - 1)$$

Ora consideriamo $A \rightarrow D \rightarrow C$

~~Isobara $A \rightarrow D$~~

~~$$\Delta U_{AD} = n c_v (T_D - T_A) = n c_v T_A (\alpha - 1)$$~~

~~$$T_D = \frac{P_D V_D}{nR} = \frac{P_A \beta V_A}{nR} = \beta T_A$$~~

Isobara $A \rightarrow D$

$$\Delta U_{AD} = n c_v (T_D - T_A) = n c_v T_A (\beta - 1)$$

$$T_D = \frac{P_D V_D}{nR} = \frac{P_A \beta V_A}{nR} = \beta T_A$$

$$Q_{AD} = n c_p (T_D - T_A) = n c_p T_A (\beta - 1)$$

$$W_{AD} = P_A (V_D - V_A) = n R (T_D - T_A) = n R T_A (\beta - 1) \stackrel{c_p = c_v + R}{=} Q_{AD} - \Delta U_{AD}$$

Isocora $D \rightarrow C$

$$\Delta U_{DC} = n c_v (T_C - T_D) = n c_v T_D (\alpha - 1) = n c_v T_A \beta (\alpha - 1)$$

$$W_{DC} = 0$$

$$Q_{DC} = \Delta U_{DC} = n c_v T_A \beta (\alpha - 1)$$

Compressivamente

$$\Delta U_{AC}^{II} = \Delta U_{AD} + \Delta U_{DC} = n c_v T_A (\beta - 1) + n c_v T_A \beta (\alpha - 1) = n c_v T_A (\alpha \beta - 1) = \Delta U_{AC}^I$$

$$Q_{AC}^{II} = n c_p T_A (\beta - 1) + n c_v T_A \beta (\alpha - 1) = n T_A [c_p (\beta - 1) + c_v \beta (\alpha - 1)] \neq Q_{AC}^I$$

$$W_{AC}^{\text{II}} = W_{AD} + W_{DC} = nRT_A(\beta-1) + 0 = nRT_A(\beta-1) \neq W_{AC}^{\text{I}}!$$

$\Delta U_{AC}^{\text{I}} = \Delta U_{AC}^{\text{II}}$ come dovrebbe essere in quanto U funzione di stato (dipende solo ~~dal percorso~~ dai punti iniziale e finale)

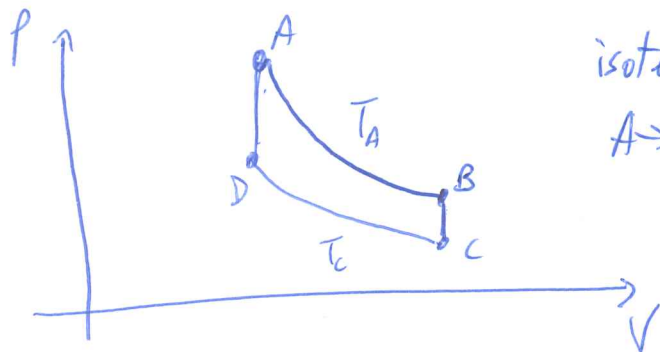
mentre $Q_{AC}^{\text{I}} \neq Q_{AC}^{\text{II}}$, $W_{AC}^{\text{I}} \neq W_{AC}^{\text{II}}$, confermando che Q e W non sono funzioni di stato, ma dipendono dal percorso seguito

Non si può parlare di Q, W posseduti, ma solo scambiati dal sistema

③

Esempio: Ciclo di Stirling

Brevettato nel 1816 dal reverendo Stirling



isoterma \rightarrow isocora \rightarrow isoterma \rightarrow isocora
 $A \rightarrow B$ $B \rightarrow C$ $C \rightarrow D$ $D \rightarrow A$
 raffreddamento riscaldamento

Isoterma $A \rightarrow B$

$$\Delta U_{AB} = 0 \quad Q_{AB} = nRT_A \ln\left(\frac{V_B}{V_A}\right) = nRT_A \ln\left(\frac{P_A}{P_B}\right) = W_{AB}$$

Isocora $B \rightarrow C$

$$W_{BC} = 0 \quad \Delta U_{BC} = nC_V(T_C - T_A) = Q_{BC}$$

Isoterma $C \rightarrow D$

$$\Delta U_{CD} = 0 \quad Q_{CD} = nRT_C \ln\left(\frac{V_D}{V_C}\right) = nRT_C \ln\left(\frac{P_C}{P_D}\right) = W_{CD}$$

Isocora $D \rightarrow A$

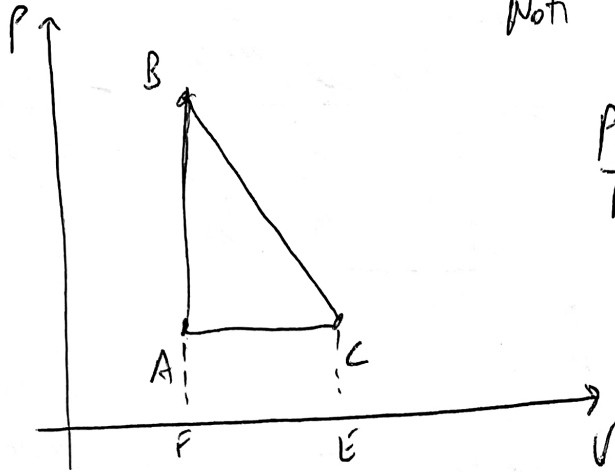
$$W_{DA} = 0 \quad \Delta U_{DA} = nC_V(T_A - T_C) = Q_{DA}$$

In totale: $\Delta U_{A \rightarrow A} = 0 + nC_V(T_C - T_A) + 0 + nC_V(T_A - T_C) = 0$

$$Q_{A \rightarrow A} = nRT_A \ln\left(\frac{P_A}{P_B}\right) + nC_V(T_C - T_A) + nRT_C \ln\left(\frac{P_C}{P_D}\right) + nC_V(T_A - T_C) = nRT_A \ln\left(\frac{P_A}{P_B}\right) + nRT_C \ln\left(\frac{P_C}{P_D}\right) = W_{A \rightarrow A}!$$

④ Ciclo "triangolare" (gas atomare)

Noti P_A, V_A, T_A



$$\frac{P_B}{P_A} = \alpha = 3$$

$$\frac{V_C}{V_A} = \beta = 2$$

AB isocora

$$Q_{AB} = nC_V (T_B - T_A) =$$

$$T_B = \frac{P_B V_B}{nR} = \alpha \frac{P_A V_A}{nR} = \alpha T_A$$

$$= nC_V (\alpha - 1) T_A = \frac{3}{2} nR T_A = 3nRT_A$$

$$\Delta U_{AB} = nC_V (T_B - T_A) = 3nRT_A$$

$$W_{AB} = \int_A^B P dV = 0$$

BC "lineare"

$$W_{BC} = \text{area trapezoid } B C E F = \frac{(P_B + P_A)(V_C - V_A)}{2} =$$

$$= \frac{(\alpha + 1) P_A (\beta - 1) V_A}{2} = \frac{(\alpha + 1)(\beta - 1)}{2} P_A V_A = \frac{(\alpha + 1)(\beta - 1)}{2} nRT_A = 2nRT_A$$

$$\Delta U_{BC} = nC_V (T_C - T_B) =$$

$$T_C = \frac{P_C V_C}{nR} = \beta \frac{P_A V_A}{nR} = \beta T_A$$

$$= nC_V (\beta - \alpha) T_A = -nC_V T_A = -\frac{3}{2} nRT_A$$

$$Q_{BC} = \Delta U_{BC} + W_{BC} = 2nRT_A - \frac{3}{2} nRT_A = \frac{1}{2} nRT_A$$

CA isobara

$$Q_{CA} = nC_P (T_A - T_C) = \frac{5}{2} nR nC_P (1 - \beta) T_A = -\frac{5}{2} nRT_A$$

$$W_{CA} = P_A \Delta V = P_A (V_A - V_C) = P_A (1 - \beta) V_A = (1 - \beta) nRT_A = -nRT_A$$

$$\Delta U_{CA} = nC_V \Delta T = nC_V (T_A - T_C) = nC_V (1 - \beta) T_A = -nC_V T_A = -\frac{3}{2} nRT_A = Q_{CA} - W_{CA}$$

$$\Delta U_{tot} = 3nRT_A - \frac{3}{2} nRT_A - \frac{3}{2} nRT_A = 0$$

$$Q_{tot} = 3nRT_A + \frac{1}{2} nRT_A - \frac{5}{2} nRT_A = nRT_A$$

$$W_{tot} = 0 + 2nRT_A - nRT_A = nRT_A = \text{area trapezoid!}$$